

## Solution2(a):

The necessary condition for the space-probe to escape from the Solar system is that the sum of its kinetic and potential energy in the Sun's gravitational field is larger than or equal to zero:

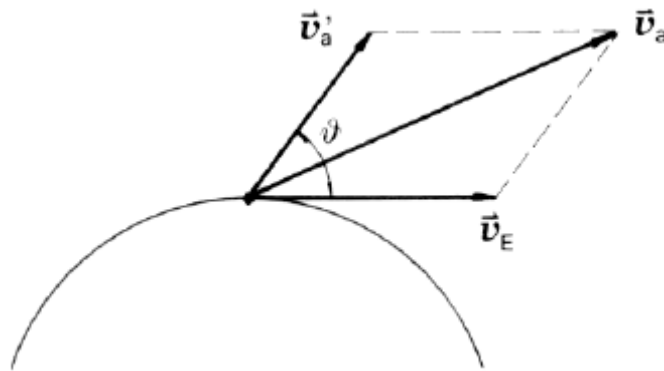
$$\frac{1}{2}mv_a^2 - \frac{GmM}{R_E} \geq 0,$$

where  $m$  is the mass of the probe,  $v_a$  its velocity relative to the Sun,  $M$  the mass of the Sun,  $R_E$  the distance of the Earth from the Sun and  $G$  the gravitational constant. Using the expression for the velocity of the Earth,  $v_E = (GM/R_E)^{1/2}$ , we can eliminate  $G$  and  $M$  from the above condition:

$$v_a^2 \geq \frac{2GM}{R_E} = 2v_E^2.$$

Let  $v'_a$  be the velocity of launching relative to the Earth and  $\vartheta$  the angle between  $\vec{v}_E$  and  $\vec{v}'_a$  (see the Figure).

Then from  $\vec{v}_a = \vec{v}'_a + \vec{v}_E$  and  $v_a^2 = 2v_E^2$  it



follows:

$$v_a'^2 + 2v'_a v_E \cos \vartheta - v_E^2 = 0$$

and

$$v'_a = v_E \left[ -\cos \vartheta + \sqrt{1 + \cos^2 \vartheta} \right].$$

(because  $-ve$  sign is not admissible.)

The minimum velocity is obtained for  $\vartheta = 0$ :

$$v'_a = v_E(\sqrt{2} - 1) = 12.3 \text{ km/s.}$$

**Solution 2(b):** The blocks slide relative to the prism with accelerations  $\mathbf{a}_1$  and  $\mathbf{a}_2$ , which are parallel to its sides and have the same magnitude  $a$  (see Fig.1). The blocks move relative to the earth with accelerations:

$$\mathbf{w}_1 = \mathbf{a}_1 + \mathbf{a}_0 \quad (1)$$

$$\mathbf{w}_2 = \mathbf{a}_2 + \mathbf{a}_0 \quad (2)$$

because the  $\mathbf{a}_0$  is the acceleration of the prism.

Now we project  $\mathbf{w}_1$  and  $\mathbf{w}_2$  along the  $x$ - and  $y$ -axes:

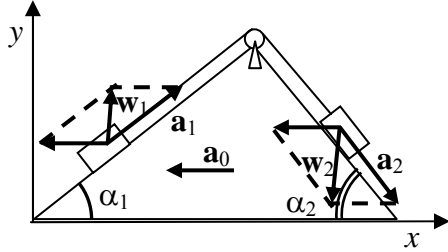


Fig.1

$$w_{1x} = a \cos \alpha_1 - a_0 \quad (3)$$

$$w_{1y} = a \sin \alpha_1 \quad (4)$$

$$w_{2x} = a \cos \alpha_2 - a_0 \quad (5)$$

$$w_{2y} = -a \sin \alpha_2 \quad (6)$$

The equations of motion for the blocks and for the prism have the following vector forms (see Fig.2):

$$m_1 \mathbf{w}_1 = m_1 \mathbf{g} + \mathbf{R}_1 + \mathbf{T}_1 \quad (7)$$

$$m_2 \mathbf{w}_2 = m_2 \mathbf{g} + \mathbf{R}_2 + \mathbf{T}_2 \quad (8)$$

$$M \mathbf{a}_0 = M \mathbf{g} - \mathbf{R}_1 - \mathbf{R}_2 + \mathbf{R} - \mathbf{T}_1 - \mathbf{T}_2 \quad (9)$$

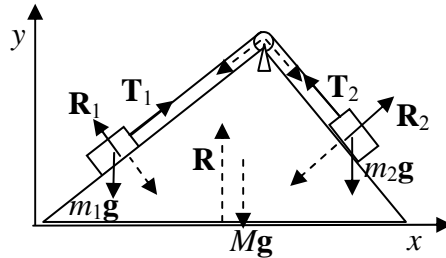


Fig.2

The forces of tension  $\mathbf{T}_1$  and  $\mathbf{T}_2$  at the ends of the thread are of the same magnitude  $T$  since the masses of the thread and that of the pulley are negligible. Note that in equation (9) we account for the net force  $-(\mathbf{T}_1 + \mathbf{T}_2)$ , which the bended thread exerts on the prism through the pulley. The equations of motion result in a system of six scalar equations when projected along  $x$  and  $y$ :

$$m_1 a \cos \alpha_1 - m_1 a_0 = T \cos \alpha_1 - R_1 \sin \alpha_1 \quad (10)$$

$$m_1 a \sin \alpha_1 = T \sin \alpha_1 + R_1 \cos \alpha_1 - m_1 g \quad (11)$$

$$m_2 a \cos \alpha_2 - m_2 a_0 = -T \cos \alpha_2 + R_2 \sin \alpha_2 \quad (12)$$

$$m_2 a \sin \alpha_2 = T \sin \alpha_2 + R_2 \cos \alpha_2 - m_2 g \quad (13)$$

$$-M a_0 = R_1 \sin \alpha_1 - R_2 \sin \alpha_2 - T \cos \alpha_1 + T \cos \alpha_2 \quad (14)$$

$$0 = R - R_1 \cos \alpha_1 - R_2 \cos \alpha_2 - M g \quad (15)$$

By adding up equations (10), (12), and (14) we get,

$$m_1 a \cos \alpha_1 - m_1 a_0 + m_2 a \cos \alpha_2 - m_2 a_0 - M a_0 \\ = T \cos \alpha_1 - R_1 \sin \alpha_1 - T \cos \alpha_2 + R_2 \sin \alpha_2 + R_1 \sin \alpha_1 - R_2 \sin \alpha_2 - T \cos \alpha_1 + T \cos \alpha_2$$

$$\text{Or,} \quad a(m_1 \cos \alpha_1 + m_2 \cos \alpha_2) = a_0(m_1 + m_2 + M)$$

$$\text{Therefore,} \quad a = a_0 \frac{M + m_1 + m_2}{m_1 \cos \alpha_1 + m_2 \cos \alpha_2} \quad (16)$$

The straightforward elimination of the unknown forces gives the final answer for  $a_0$ :

$$a_0 = \frac{(m_1 \sin \alpha_1 - m_2 \sin \alpha_2)(m_1 \cos \alpha_1 + m_2 \cos \alpha_2)}{(m_1 + m_2 + M)(m_1 + m_2) - (m_1 \cos \alpha_1 + m_2 \cos \alpha_2)^2}. \quad (17)$$

It follows from equation (17) that the prism will be in equilibrium ( $a_0 = 0$ ) if:

$$\frac{m_1}{m_2} = \frac{\sin \alpha_2}{\sin \alpha_1}. \quad (18)$$

**Solution 3(a) :** We use the following notation:

$t$	temperature of the final equilibrium state,
$t_0 = 0^\circ\text{C}$	the melting point of ice under normal pressure conditions,
$M_2$	final mass of water,
$M_3$	final mass of ice,
$m'_2 \leq m_2$	mass of water, which freezes to ice,
$m'_3 \leq m_3$	mass of ice, which melts to water.

a) Generally, four possible processes and corresponding equilibrium states can occur:

(i).  $t_0 < t < t_2$ ,  $m'_2 = 0$ ,  $m'_3 = m_3$ ,  $M_2 = m_2 + m_3$ ,  $M_3 = 0$ .

Unknown final temperature  $t$  can be determined from the equation

$$(m_1 c_1 + m_2 c_2)(t_2 - t) = m_3 c_3(t_0 - t_3) + m_3 l + m_3 c_2(t - t_0) \quad (1)$$

However, only the solution satisfying the condition  $t_0 < t < t_2$  does make physical sense.

(ii).  $t_3 < t < t_0$ ,  $m'_2 = m_2$ ,  $m'_3 = 0$ ,  $M_2 = 0$ ,  $M_3 = m_2 + m_3$ .

Unknown final temperature  $t$  can be determined from the equation

$$m_1 c_1(t_2 - t) + m_2 c_2(t_2 - t_0) + m_2 l + m_2 c_3(t_0 - t) = m_3 c_3(t - t_3) \quad (2)$$

However, only the solution satisfying the condition  $t_3 < t < t_0$  does make physical sense.

(iii).  $t = t_0$ ,  $m'_2 = 0$ ,  $0 \leq m'_3 < m_3$ ,  $M_2 = m_2 + m'_3$ ,  $M_3 = m_3 - m'_3$ .

Unknown mass  $m_3$  can be calculated from the equation

$$(m_1c_1 + m_2c_2)(t_2 - t_0) = m_3c_3(t - t_3) + m'_3l \quad (3)$$

However, only the solution satisfying the condition  $0 \leq m'_3 \leq m_3$  does make physical sense.

(iv).  $t = t_0$ ,  $0 \leq m_2 \leq m_2$ ,  $m'_3 = 0$ ,  $M_2 = m_2 - m'_2$ ,  $M_3 = m_3 + m'_2$ .

Unknown mass  $m_2$  can be calculated from the equation

$$(m_1c_1 + m_2c_2)(t_2 - t_0) + m'_2l = m_3c_3(t_0 - t_3) \quad (4)$$

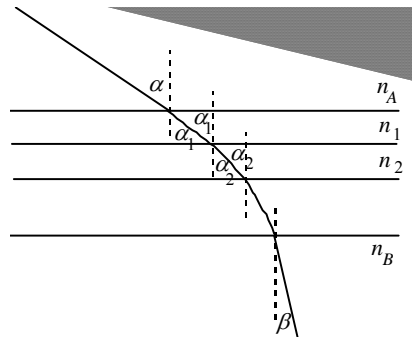
However, only the solution satisfying the condition  $0 \leq m'_2 \leq m_2$  does make physical sense.

b) Substituting the particular values of  $m_1$ ,  $m_2$ ,  $m_3$ ,  $t_2$  and  $t_3$  to equations (1), (2) and (3) one obtains solutions not making the physical sense (not satisfying the above conditions for  $t$ , respectively  $m'_3$ ). The real physical process under given conditions is given by the equation (4) which yields

$$m_2 = [m_3c_3(t_0 - t_3) - (m_1c_1 + m_2c_2)(t_2 - t_0)]/l$$

Substituting given numerical values one gets  $m_2 = 0.11$  kg. Hence,  $t = 0^\circ\text{C}$ ,  $M_2 = m_2 - m'_2 = 0.89$  kg,  $M_3 = m_3 + m_2 = 2.11$  kg.

**Solution 3(b) :**



Let us divide the plate in a large number of small slides as shown in the figure such that one can assume that the light ray travels in a straight line within each small slide  $n_1$ ,  $n_2$ , ..... ,  $n_m$  so that one can take refractive index constant within the small slide.

Then from the figure, we get,

$$n_A \sin \alpha = n_1 \sin \alpha_1 = n_2 \sin \alpha_2 = \dots = n_B \sin \beta$$

Or,  $n_A \sin \alpha = n_B \sin \beta$ .

**Solution 4(a) :** A circuit equivalent to the given one is shown in Fig.3. In a steady state (the capacitors are completely charged already) the same current  $I$  flows through all the resistors in the closed circuit ABFGHDA. From the Kirchhoff's second rule we obtain:

$$I = \frac{E_4 - E_1}{4R}. \quad (1)$$

Next we apply this rule for the circuit ABCDA:

$$V_1 + IR = E_2 - E_1, \quad (2)$$

where  $V_1$  is the potential difference across the capacitor  $C_1$ . By using the expression (1) for  $I$ , and the equation (2) we obtain:

$$V_1 = E_2 - E_1 - \frac{E_4 - E_1}{4} = 1 \text{ V}. \quad (3)$$

Similarly, we obtain the potential differences  $V_2$  and  $V_4$  across the capacitors  $C_2$  and  $C_4$  by considering circuits BFGCB and FGHEF:

$$V_2 = E_4 - E_2 - \frac{E_4 - E_1}{4} = 5 \text{ V}, \quad (4)$$

$$V_4 = E_4 - E_3 - \frac{E_4 - E_1}{4} = 1 \text{ V}. \quad (5)$$

Finally, the voltage  $V_3$  across  $C_3$  is found by applying the Kirchhoff's rule for the outermost circuit IJEHLKDAI:

$$V_3 = E_3 - E_1 - \frac{E_4 - E_1}{4} = 5 \text{ V}. \quad (6)$$

The total energy of the capacitors is expressed by the formula:

$$W = \frac{C}{2} (V_1^2 + V_2^2 + V_3^2 + V_4^2) = 26 \text{ } \mu\text{J}. \quad (7)$$

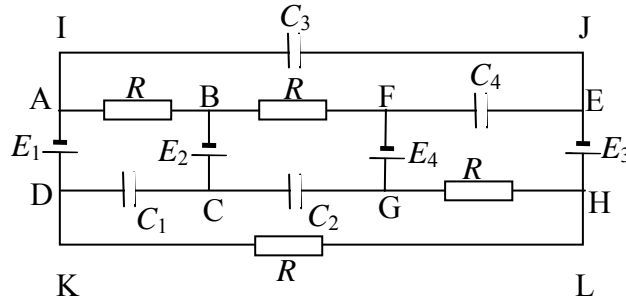


Fig. 3

When points B and H are short connected (circuited) the same electric current  $I'$  flows through the resistors in the BFGH circuit. It can be calculated, again by means of the Kirchhoff's rule, that:

$$I' = \frac{E_4}{2R}. \quad (8)$$

The new steady-state voltage on  $C_2$  is found by considering the BFGCB circuit:

$$V_2' + I'R = E_4 - E_2 \quad (9)$$

or finally:

$$V_2' = \frac{E_4}{2} - E_2 = 0 \text{ V}. \quad (10)$$

Therefore the charge  $q'_2$  on  $C_2$  in the new steady state is zero.

**Solution 4(b)** : (i) By Gauss's law,  $\sigma = \epsilon_0 E_0$ , for a plane surface,



where  $\sigma$  is the Earth's surface charge density,  $\epsilon_0$  is the permittivity of the free space and  $E_0$  is the electric field at the Earth's surface. Therefore,  $\sigma = -8.85 \times 10^{-12} \times 150$   
 $= -1.33 \times 10^{-9} \text{ C/m}^2$ . (1)

And total charge carried on the Earth's surface ( $Q$ ) =  $4\pi R^2 \sigma$   
 where  $R$  is the radius of the Earth. Therefore, using (1), we get,  
 $Q = -4\pi \times (6.4 \times 10^6)^2 \times 1.33 \times 10^{-9} \text{ C} \approx -6.7 \times 10^5 \text{ C}$ .

(ii) Consider a cylinder of cross section  $A$  with faces at heights of 0 and 100 m.  
 By Gauss's law,  $E(0) A - E(100) A = q_{\text{enclosed}} / \epsilon_0 = \rho_{\text{ave.}} \cdot (100A) / \epsilon_0$

Therefore,  $\rho_{\text{ave.}} = \epsilon_0 [E(0) - E(100)] / 100$   
 $= 8.85 \times 10^{-12} [150 - 100] / 100 \approx 4.43 \times 10^{-12} \text{ C/m}^3$

